

The Kobelco Arc: Our Promise to Create the Future

KOBELCO Group News

A Big Stride Expected for a New Era at INTIWI

After Mr. Dahlan Gunawan s retirement in 1999, I succeeded him as President Director of P. T. INTAN PERTIWI INDUSTRY (INTIWI). In the early years of my new assignment, I had so much to learn about the other side of the company which differed so much from the factory side, where I had been stationed as general manager for over two decades. Fortunately, my staff in the head office is already familiar with their work, and daily activities can go on without much difficulty. Besides, the majority of the factory workers have been working for the company for ages, during which they have acquired the tight scrutiny of quality control practiced in the production line. With such talented office staff and competent factory workers, the transition period in my new assignment has passed smoothly and the business is going on as I expect.

During these four years, I have found very good business relationships between our company and Kobe Steel, Thai-Kobe Welding and Kobe Welding Singapore due to their very positive and warm attitudes. Early this year the license agreement with Kobe Steel was renewed, thereby allowing Kobelco welding electrodes to remain as the market leader in Indonesia to respond to demands for high quality products in the welding electrodes market. The license agreement also reflects the strong bond between licensor and licensee built on mutual trust and benefit. With the help of the Technical Development Department of Kobe Steel, INTIWI s production line is now being modified to maximize the production capacity, thereby enhancing the production efficiency.



From the top, my staff and I posing in front of the factory, discussing in a meeting room, and attending the operation for chemical analysis for quality control

In early November 2002, our company celebrated our 25th anniversary. Time really flies - I never felt I had already worked for the company for 25 years since I joined. During the anniversary, we had a small party, at which all factory workers and head office staff had lunch, danced and socialized. Many of the employees joined our company when they were single and now they have families. Workers who are reaching retirement age even recommend their sons or daughters to take up some positions in our company. As such our employees are loyal to INTIWI.

As the Indonesian economy is now showing some sign of recovery, our sales volume has been picking up approximately 80% of the normal sales volume since the currency crisis in 1997. This year s business performance is expected to be quite satisfactory, despite the detrimental effect of a few acts of terrorism that happened locally and the Iraq war, during which the economy was very sluggish. However, we anticipate that sales will be affected temporarily next year, because there will be a national election and new projects may get started. If the election will go on well and a new government will be accepted by the people, we predict that the economy will continue to recover and investors will start coming to Indonesia. Most of the people also would want the economy to recover so as to absorb the many jobless people in the country. We hope that is when we will see demand for welding electrodes surge.

Lastly, when I think of our company s successful trend over a quarter century, I really hope that better futures will come to us, and Kobelco welding electrodes, with unsurpassed innovative quality, will grow its market niche in Indonesia.

Preface

Message from the Editor

Dear Readers:

How are you these days? It was unusually cool this summer in Japan. In contrast, the summer in Europe was extremely hot. Nowadays people are facing unconventional weather throughout the world. Earth seems somehow to be changing its nature, affected by extraordinary global events." Everybody loves somebody sometimes.... "If people would love our life-and-death planet, we would be able to sustain the globe in its conventional natural condition because everybody loves such natural things as deep-blue sea, blue sky, and green forest.

KOBELCO s newest plant in China, KOBE WELDING OF TANGSHAN has started to produce solid wires. The Chinese market for welding consumables is growing every year in tandem with the country s economic growth. I believe this company will be able to contribute, with their quality products and technical services, to a lot of fabricators in China. Whenever we promote the globalization of our business, we remind ourselves that globalization accompanies localization. Globalization makes us realize that there are so many different local needs in individual markets. Globalization also requires us to overcome our cross-cultural problems. I am affected in my humanity by different cultures every time when I met people in different countries.

Calling from Tokyo

Hello, KWT readers worldwide:

Hui Ding is my name. I am engaged in exporting welding consumables to the Chinese market. I entered Kobe Steel and was assigned to the present department 6 years ago, when the first issue of Kobelco Welding Today was just published. Therefore, KWT magazine and I are, so to speak, colleagues in terms of our period of engagement. This magazine is distributed to customers in the Chinese market, where it enjoys a reputation as high as that in other countries. I will maximize the competence of this dependable colleague, expecting expanded sales of welding consumables in China.

Two years have passed since I took charge of exporting welding consumables to the Chinese market. Keeping in mind a Japanese proverb," Perseverance for at least three years brings success, "I will make every endeavor to provide customers with more satisfaction through my services.

Have a good day.

Hui Ding International Operations Dept. Welding Company Kobe Steel, Ltd.



Masakazu Tojo Editorial Chairman

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Kobelco SAW Fluxes/Wires Cover a Wide Scope of Heavy Fabrication Industries



Submerged arc welding (SAW), a typical automated welding technique, is widely used for fabricating hulls, pressure vessels, storage tanks, architectural structures, bridges, pipelines, and construction equipment. Its popularity is due to high deposition rates and deep penetration that are beneficial in welding medium-thick and thick sections. The process is limited generally to the flat and horizontal fillet positions because of the flux used to shield the weld puddle. However, with special flux dams, it can be used in the horizontal groove weld position as in joining the shells of cylindrical storage tanks.

The welding consumables required are consumable electrode and granular flux. The electrodes vary in shape - solid wire, flux cored wire, and strip - and in application - carbon steel, low alloy steel, stainless steel, nickel-based alloy, and hardfacing. The fluxes can be classified into three significantly different types: fused, bonded, and agglomerated fluxes.

Three Types of Kobelco SAW Fluxes: Fused, Bonded, and Agglomerated

Fused fluxes are produced by dry mixing aggregated or granular mineral, followed by melting at one thousand or higher degrees Celsius in an electric furnace. The molten material is cooled rapidly to its solid state and processed to produce the desired particle size. Depending on the process, the particles in the fused flux can be glassy or porous. The particles result in a variety of sizes so as to maximize the performance of the flux with varied welding currents.

Bonded fluxes are produced by dry mixing powdered mineral and, if needed by the application, metal. This is followed by wet mixing with bonded agents.

This wet-mixed material is then pelletized, baked at a

temperature (e.g. 400-550) below its melting point, and then processed to produce the desirable particle sizes.

Agglomerated fluxes are produced with a bonded agent requiring a higher baking temperature (e.g. 700-1000). The production process of this type of flux is similar to that of the bonded type except for the binding agent and baking temperature. This is followed by processing to produce the most desirable particle size.

Solid Wires for General Uses; Flux-Cored Wires and Strips for Specific Applications

Kobelco SAW solid wires differ in chemistry and size to respond to demands from such heavy fabrication industries as shipbuilding, steel structure and bridge construction, and pressure vessel, storage tank and pipeline fabrication. Kobelco flux-cored wires for SAW are available for hardfacing steel mill rollers and construction machinery. Strip electrodes available from Kobelco are for stainless steel and nickel-based alloy overlaying and hardfacing.

Higher Efficiency Welding Achieved with Kobelco s Varied SAW Flux-Wire Combinations

Tables 1 through **4** show how Kobelco s diverse SAW fluxes (available for overseas markets) can be combined with different solid wires and flux-cored wires according to the applications. Many fluxes can be combined with different wires for welding several types of base metals, but some fluxes require a specific wire for welding a specific type of base metal. For details of Kobelco SAW flux-wire and flux-strip combinations, please refer to KOBELCO WELDING HANDBOOK.

Table 1. Kobelco flux/wire varieties for mild steel, high tensile steel, low temp. steel and heat-resistant low-alloy steel

| Flux | Flux/wire | Wire | Ir | Flux size | | |
|------------------------|--------------------------------|---|--|---|---|--|
| brand (1) | AWS class. | brand ⁽²⁾ | Base metal | Features ⁽³⁾ | (Mesh) | |
| AF-490 | F7A4-EM12K F6P6-EM12K | US-12K | | For multi-pass welding Only DC-EP is applicable | 10 × 48 | |
| G-50 | F7A2-EH14 | | For thin plates with high speeds DC-EP is better for sheet metals | | | |
| G-60 | F7A2-EH14 | US-36 | | For thin or medium-thick plates with high speeds | 12×65, 12×150 | |
| G-80 | F7A2-EH14 F6P2-EH14 | | Mild steel, 490MPa HT steel | For multi-pass welding of medium or heavy thick plates Good mechanical properties | 12 × 65, 12 × 120, 20 × 200, 32 × 200, 20 × D | |
| MF-300 | F7A6-EH14 F7P6-EH14 | US-36 | | For multi-pass welding of Medium or heavy thick plates Excellent slag removal and good mechanical properties | 20 x 200, 20 x D | |
| | F7A6-EH14 F7P6-EH14 | US-36 | Mild steel, 490MPa HT steel | Good performance in horizontal vertical welding of storage tanks DC-EP current is suitable | | |
| MF-33H | H F8A6-EG-A4 US-49 | | 550-610MPa HT steel | Good performance in horizontal vertical welding of storage tanks DC-EP current is suitable | 12 x 150 | |
| F7A6-EH14 F7P6-EH14 | | US-49A | Low temp. steel | Good performance in horizontal vertical welding of storage tanks DC-EP current is suitable | | |
| | F7A6-EH14 F7P6-EH14 US-36 M | | Mild steel 490MPa HT steel | For multi-pass welding of medium or heavy thick plates Excellent mechanical properties | | |
| - | F7A2-EG-G | USW-52B | | For non-postweld-painting applications Good impact value | | |
| | F8A2-EG-G | USW-62B | Weather proof steel | For non-postweld-painting applications Good mechanical properties | | |
| | F8A4-EW-W | USW-588 | | Suitable for ASTM A588 steel | 12 × 65, | |
| ME-29 | F8A4-EG-A4 F8P6-EG-A4 US-49 | | 550-590MPa HT | Suitable for 0.5% Mo steel | 20 × 200, 20 × D | |
| 1011-50 | F8A4-EA4-A4 F8P6-EA4-A4 | US-A4 | Iow-alloy steel Suitable for 0.5% Mo steel | | | |
| | F9A6-EA3-A3 F8P6-EA3-A3 | US-40 | 550-610MPa HT steel, Heat-resist. low-alloy steel | Suitable for 0.5% Mo steel | | |
| | F7A6-EH14 F7P6-EH14 | US-49A | Low temp. steel | Excellent impact value at - 40 or higher | | |
| | - US-36 | | Mild steel | For FAB one-side welding with FAB-1 backing and RR-2 metal powder | 20 × 200 | |
| | - | US-49 | 490MPa HT steel | For FAB one-side welding with FAB-1 backing and RR-2 metal powder | 1 20 × 200 | |
| MF-38A | F7A2-EG-G | USW-52B | Weather proof steelFor non-postweld-painting applicationsGood bead appearance | | 12×65, 20×200 20×D | |
| | F7AO-EH14 | US-36 | Mild steel, 490MPa HT steel | Excellent bead appearance and slag removal in fillet welding | | |
| MF-53 | F7A0-EG-G | USW-52B Weather proof steel For non-postweld-paintin Excellent bead appearain fillet welding | | For non-postweld-painting applications Excellent bead appearance and slag removal in fillet welding | 8 x 48 | |
| MF-63 | F8A0-EG-G | USW-62B | Weather proof steel | For non-postweld-painting applications 8 × 48 | | |

Note: (1) The initial letter of brand names designates the type of flux - A: agglomerated, and G/M: fused. (2) Solid wire. (3) Unless polarity is otherwise mentioned, AC current is recommended.

Table 1 (cont.). Kobelco flux/wire varieties for mild steel, high tensile steel, low temp. steel and heat-resistant low-alloy steel

| Flux | Flux/wire | Wire | | Intended usage and features | Flux size | |
|--|------------------------|--------------------------|---|--|----------------|--|
| brand ⁽¹⁾ | AWS class. | brand ⁽²⁾ | Base metal | Features (3) | (Mesh) | |
| PFH-45 | F6A4-EL8 | US-43 | | For single-pass-double-sided or multi-pass welding Excellent bead appearance with high currents | 10 x 48 | |
| PFH-55E | F7A4-EH14 | US-36 | Mild steel, 490MPa HT steel | For single-pass-double-sided or multi-pass welding Good bead appearance and excellent impact value | 10 x 48 | |
| PFH-55AS | F7A8-EH14 F7P8-EH14 | US-36J | | Only DC-EP current is applicable Excellent impact value at - 60 or higher and CTOD at - 20 or higher | 10 x 48 | |
| PFH-55LT | F7A8-EH14 F7P8-EH14 | US-36 | Low temp. steel | Only AC current is applicable Excellent impact value at - 60 or higher and CTOD at - 50 or higher | 10 x 48 | |
| PFH-60A | F7A4-EL8 | US-43 | Mild steel, 490MPa HT steel | For single-pass-double-sided or multi-pass welding POMPa HT steel Excellent bead appearance with high currents | | |
| | F12A10-EG-G | US-80LT | | Only AC current is applicable Excellent impact value at - 80 or higher | | |
| PFH-80AK F11A4-EG-G US-80BN | | 780MPa HT steel | Excellent bead appearance and slag removal Only AC current is applicable | 1 IU x 48 | | |
| PFH-80AS | F11A10-EG-G | US-80LT | 780MPa HT steel | Only DC-EP current is applicable Excellent impact value at - 80 or higher | 10 x 48 | |
| PFH-203 | F7P15-ENi3-Ni3 | US-203E | 3.5%Ni steel | Excellent impact value at - 100 or higher after PWHT | 10 x 48 | |
| PFI-50 | - | US-43 | | For FCB one-side welding with PHI-50R or MF-1R backing flux | 10 x 48 | |
| PFI-52E | - | US-36 | Mild steel, 490MPa HT steel | For FAB one-side welding with FAB-1 backing and RR-2 metal powder | 10 x 48 | |
| PFI-55E | - | US-36 | | For FCB one-side welding with PHI-5OR or MF-1R backing flux | 10 x 48 | |
| MF-27 | F9P4-EG-G | US-56B | Mn-Mo steel, Mn-Mo-Ni steel | Excellent crack resistance and notch toughness | 48 x D | |
| | F7PZ-EG-B2 | US-511 | 1-1.25%Cr- 0.5%Mo steel | AC current is suitable Good crack resistance | 40.5 | |
| IVIF-29A | F8P2-EG-B3 | US-521 | 2.25%Cr- 1%Mo steel | AC current is suitable Good crack resistance | - 48 X D | |
| | F8P2-EG-B2 | US-511N | 1-1.25%Cr- 0.5%Mo steel | AC current is suitable Excellent notch toughness | | |
| PF-200 F9P2-EG-B3 | | US-521S | 2.25%Cr- 1%Mo steel | AC current is suitable Excellent notch toughness | 10 × 48 | |
| F9P4-EG-G US-56B | | US-56B | Mn-Mo steel, Mn-Mo-Ni steel | Excellent crack resistance and notch toughness | | |
| F7P2-EG-B6 US-502 5%Cr-0.5%Mo Good crack resista | | Good crack resistance | 10 10 | | | |
| PF-200S | F10PZ-EG-G | vZ-EG-G US-9Cb 9% | | AC current is suitable Excellent creep rupture strength | 10×48 | |
| PF-500 | - | US-521H | 2.25%Cr-1%Mo-V steel | AC current is suitable Excellent creep rupture strength | 10 x 48 | |
| PF-500D | - | US-521HD | 2.25%Cr-1%Mo-V steel | Excellent high temp. properties with DC-EP currents | 10 x 48 | |

Note: (1) The initial letter of brand names designates the type of flux - P: bonded, and M: fused. (2) Solid wire (3) Unless polarity is otherwise mentioned, AC current is recommended.

Table 2. Kobelco flux/wire varieties for stainless steels

| Flux | Flux Wire Wire | | Intended usage | Flux size | |
|--------------------------------|-----------------------|-------------------|--|-----------------------------|----------------|
| brand ⁽¹⁾ | brand ⁽²⁾ | AWS class. | Base metal | Features ⁽³⁾ | (Mesh) |
| | US-308 | ER308 | 304 steel | Good crack resistance | |
| | US-308L | ER308L | 304L steel | Better corrosion resistance | |
| US-309 | | ER309 | 309 and 309S steel | Good weldability | 10 |
| PF5-1 | US-309L ER309L | | 309 and 309S steel | Good weldability | 12×05 |
| | US-317L ER317L | | 316LN and 317L steel Good weldability | | |
| US-347 ER347 347 and 321 steel | | 347 and 321 steel | Good weldability | | |
| PFS-1LT | US-308L | ER308L | 304 and 304L steel Excellent notch toughness | | 12 × 65 |
| | US-316 | ER316 | 316 steel | Good crack resistance | 10/ 5 |
| PFS-TIM | US-316L | ER316L | 316L steel | Better corrosion resistance | 12×05 |
| PFS-4M | US-410 | - | 403, 410, 410S, 410L, and 405 steel Good weldability | | 12×65 |

Note: (1) Bonded type flux. (2) Solid wire.

(3) Both AC and DC-EP currents are suitable; however, DC-EP is recommended for small dia. wires (2.4 mm).

Table 3. Kobelco flux/wire varieties for 9%Ni steel

| Flux | Wire | Wire | | Flux size | |
|----------------------|---|------|------------|---|----------------|
| brand ⁽¹⁾ | d ⁽¹⁾ brand ⁽²⁾ AWS class. Base metal F | | Features | (Mesh) | |
| PFN-3 | 115 2005 | | 9%Ni steel | Ni-based alloy weld metal Excellent usability and crack resistance For flat position welding Both AC and DC-EP currents are suitable | 12 × 65 |
| PFN-4 | US-709S ERNiMo-8 | | 9%Ni steel | Ni-based alloy weld metal Excellent usability and X-ray soundness For horizontal groove and fillet welding For DC-EP current | 12 × 65 |

Note: (1) Bonded flux. (2) Solid wire.

Table 4. Kobelco flux/wire varieties for hardfacing

| Flux | Wire | Nominal | | Intended usage and applications | | | |
|---------------------------------------|----------------------|----------|-------------------------------|--|------------------|--|--|
| brand ⁽¹⁾ | brand ⁽²⁾ | hardness | Type of wear Applications (3) | | (Mesh) | | |
| USH-250 | | Hv 250 | Metal-to-metal | Wheels, rollers, and tractor idlers | | | |
| | USH-350N | Hv 350 | wear | Tractor idlers and links, shovels, steel mill rollers, tires | 8 × 48 | | |
| G-50 USH-400 USH-450 USH-500 | USH-400N | Hv 400 | | Tractor idlers and links, shovels, steel mill rollers, tires | | | |
| | USH-450N | Hv 450 | Metal-to-metal | Tractor rollers and idlers, shovels, steel mill rollers, blast furnace bells | | | |
| | USH-500N | Hv 500 | and abrasive wear | Tractor rollers and idlers, shovels, steel mill rollers, blast furnace bells | | | |
| ME 20 | USH-550N | Hv 550 |] | Steel mill rollers, blast furnace bells | 10 / 5 | | |
| IVIF-30 | USH-600N | Hv 600 | | Steel mill rollers (Photo 1), crusher cones | 7 12 x 65 | | |

Note: (1) Fused flux. (2) Flux-cored wire. (3) Both AC and DC-EP currents are suitable.

Photo 1. Hardfacing a steel mill roller by paralleled SAW with MF-30/USH-600N



Outstanding Characteristics of Kobelco Agglomerated Flux: AF-490

As shown in **Photo 2**, AF-490 (AWS A5.17 F7A4-EM12K, F6P6-EM12K) flux offers more regular bead appearance and superior slag removal over a wider range of welding speeds or heat input, when compared with conventional agglomerated fluxes that have typically been used in steel structures worldwide. In addition, in combination with US-12K (AWS A5.17 EM12K) solid wire, AF-490 provides unsurpassed absorbed energy in impact testing of the weld metal in the as-welded and postweld heat treated conditions as illustrated in **Fig. 1**.



Photo 2. Joint penetration and bead appearance of AF-490/US-12K weld joints by single-pass-double-sided welding (700-750A/32-33V/40-80CPM)



Figure 1. Impact test results of AF-490/US-12K multi-pass weld metal in the as-welded and PWHT (620 × 1hr) conditions

With such excellent usability and mechanical properties, AF-490/US-12K should be used in a wide range of applications for mild steel and 490-MPa high strength steel including single-pass-double-sided welding in hulls and fillet welding in architectural structures and bridges.

A Revolutionary SAW Process: High-Speed FCB One-Run Welding

The Flux Copper Backing (FCB) one-run process developed by Kobe Steel has been a standard SAW process for single-sided welding of hull plates at high travel speeds in shipbuilding worldwide since its inception in 1965. However, users have desired that the FCB process enhance productivity more efficiently to cope with increased fabrication costs caused by the requirements for double hulled oil tankers.

The development of Ti-B micro-alloyed PFI-55E flux has increased FCB process efficiency over the conventional flux, as shown in **Fig. 2**. This advantage is derived from 20% higher deposition rates, applicability of a four-wire process and consistent bead appearance over a wide range of welding parameters, which in turn has made applicable plate thickness range as wide as 10-40 mm in one-run SAW. In addition, higher travel speeds decrease heat input by 10%, thereby improving the mechanical properties of the weld metal and heat affected zone and decreasing welding distortion. The mechanical properties of PFI-55E/US-36 meet the ship class grade-3 requirements.



Figure 2. Proper travel speed as a function of plate thickness for high-speed FCB process in comparison with conventional FCB process

Unmatched Performance with DC-EP Currents in Low Temperature Applications

A flux/wire combination of PFH-55AS/US-36J has been developed so as to possess mechanical properties similar to those of traditional PFH-55LT/US-36 but its welding performance has been modified to suit DC-EP current that is most often used overseas though not in Japan. Ti-B micro-alloyed PFH-55AS/US-36J offer, in both as-welded and postweld heat treated conditions, consistent room temperature tensile properties and low temperature notch toughness at - 60 as shown in **Fig. 3** and CTOD values at - 20 (**Table 5**), due to fine grained acicular ferrite microstructure of the weld metal - **Photo 3**.



Figure 3. Mechanical properties of PFH-55AS/US36J weld metal as a function of PWHT parameter

| 17.1: 580 | x 1hr, 17.5: 600 | x 1hr, 17.9: 620 | x 1hr |
|-----------|-------------------------|-------------------------|-------|
| 18.5: 620 | x 5hr. 18.8: 620 | × 10hr, 19,1; 650 | × 5h |

Table 5. CTOD values of PFH-55AS/US-36J weld metal

| Base metal | | PWHT | Test temp. | CTOD (mm) | |
|------------|----------------|-----------|------------|------------------|--|
| | BS4360 Gr. 50D | As-welded | - 20 | 1.10, 1.10, 1.00 | |
| | T: 70 mm | 620 × 3hr | - 20 | 1.06, 1.59, 1.31 | |

Note: Testing method: BS standard

Photo 3. Fine grained acicular ferrite microstructure of Ti-B micro-alloyed PFH-55AS/US-36J weld metal (as-welded)



Tips for Successful SAW

1. Power source polarity

The particular combination of flux and wire generally determines the choice of AC or DC in SAW. With DC-EP, the flux consumption ratio is roughly 10-30% higher than with AC depending on the type of flux. Consequently, the chemistry - and thus the mechanical properties - of the weld metal can be affected by the polarity to a high or low degree depending on the type of flux. This is why, where the quality requirement is stringent, a careful combination of flux and wire is necessary in consideration of the polarity of the power source to be used.

2. Recycling flux

The unfused part of the flux distributed around the arc is commonly recovered for reuse; however, recovered flux can be contaminated with ferric oxides and changed in grain size, which may affect the usability of the flux and quality of the weld metal when the use of recycled flux is excessive. To maintain good performance of a flux, an appropriate amount of virgin flux should be added to the retrieved flux. It is recommended that the recycling of flux be limited to a total number of three times as a rule of thumb.

3. Redrying flux

Regardless of the type of flux - fused, bonded and agglomerated - fluxes can absorb moisture at a high or low rate, even though some particular brands of flux offer moisture resistance. Therefore, it is recommended that any flux be redried before use to recover the desired usability of the flux and to decrease diffusible hydrogen in the weld metal, in accordance with the manufacturer s' specification as shown in **Table 6** for example.

| | Table 6. | Proper | redrying | conditions | for | Kobelco | fluxes |
|--|----------|--------|----------|------------|-----|---------|--------|
|--|----------|--------|----------|------------|-----|---------|--------|

| Type of flux | Brand | Drying temp. | Drying time |
|--------------|----------------------|--------------|-------------|
| Fused | All brands | 150-350 | 1 hr |
| Bonded | PFH-80AK PFH-80AS | 250-350 | 1 hr |
| | Other brands | 200-300 | 1 hr |
| Agglomerated | AF-490 | 200-300 | 1 hr |

4. Depth of flux layer

The depth of the flux layer affects the appearance and soundness of the weld. If the flux layer is excessively deep, the bead appearance becomes irregular and slag inclusions will degrade the soundness. Conversely, if the flux depth is excessively shallow, flashing and spattering will occur, resulting in poor bead appearance and X-ray soundness.

DWA-81N11 AWS A5.29 E81T1-Ni1MJ

A Brand New Flux-Cored Wire for Low Temperature Applications

DWA-81Ni1 resembles DWA-55L, sharing a similar rutile-based flux core, suitable shielding gas (80% Ar-20% CO₂), tensile strength and notch toughness of aswelded weld metal. However, their chemical compositions - and thus their AWS classifications - are different, and only DWA-81Ni1 is suited to postweld heat treatment (PWHT). The nickel content of DWA-81Ni1 weld metal is nominally 1% and notch toughness can be kept sufficient even after PWHT.

The low Ni content and PWHT applicability can be advantages in specific fabrications - such as those that adhere to the NACE standard which requires the weldment to be low in Ni content and hardness for minimizing the susceptibility to sulfide stress corrosion cracking (SSCC) that tends to occur in corrosive, aqueous H₂S environments. Such specific fabrications can be involved in offshore structures and floating production, storage and offloading vessels (**Photo 1**). Many low-alloy steels used in such applications may require PWHT to temper or relieve stresses in the weld to achieve increased ductility.

Table 1 shows typical chemical composition and tensile properties of DWA-81Ni1 welded on high strength FH36 grade steel of LR ship class. The tensile properties of the weld metal meet the requirements (0.2%OS 355MPa, TS: 490-620, El 21%) of this steel grade. Ti-B micro-alloying is one of the features of the chemical composition of the weld metal, which contributes to fine grain acicular ferrite microstructure (**Photo 2**) and in turn excellent notch toughness with minimized SR embrittlement as shown in **Figure 1** and CTOD values - **Table 2**.

| Chemical composition of weld metal (%) | | | | | | | | | | |
|--|----------------------------------|-------|-----|-------|-------|----|------|-----|-------|--------|
| С | S | i I | Mn | Р | \$ | 5 | Ni | | Ti | В |
| 0.049 | 0.3 | 31 1 | .25 | 800.0 | 0.007 | | 0.96 | 5 C | 0.046 | 0.0057 |
| | Tensile properties of weld metal | | | | | | | | | |
| Welding | | PWHT | | 0.2% | os | Т | S | E | El | RA |
| positi | on | | | | a) | (M | Pa) | (% | 6) | (%) |
| Horizontal | | As we | eld | 581 | | 60 | 04 | 2 | 5 | 68 |
| | | 580 | ×2h | 533 | 3 | 59 | 96 | 2 | 6 | 63 |
| Vertical | | As we | eld | 544 | 1 | 60 | 04 | 2 | 7 | 71 |
| | | 580 | ×2h | 509 |) | 59 | 91 | 3 | 0 | 71 |

Note: (1) Specimen location: final side



Photo 2. Fine microstructures of DWA-81Ni1 as-welded weld metal on the final side in vertical position



Figure 1. Absorbed energies in Charpy impact testing of DWA-81Ni1 weld metal in the as-welded and PWHT (580 $\,$ x 2h) conditions

Base metal: 50-mm thick FH36 Groove: double-bevel Specimen location: final side

 Table 2. CTOD values of DWA-81Ni1 weld metal in the as-welded condition

| Base metal | PWHT | Test temp. | CTOD (mm) |
|------------------|------------|------------|------------------|
| FH36 T: 50 mm | Horizontal | - 10 | 0.38, 0.38, 0.38 |
| | Vertical | - 10 | 0.65, 0.76, 0.77 |

Note: Testing method: BS standard (W = 2B)

Thomas Medal is Awarded to the Best Contributor to International Standardization for Welding Consumables

The International Institute of Welding (IIW) awarded the" Thomas Medal "to Mr. Shinsuke Tsutsumi, a senior researcher of the Technical Development Dept. of Kobe Steel Welding Company, in the Opening Ceremony of the 56th IIW Annual Assembly held in Bucharest of Rumania on July 6, 2003.



The Thomas Medal was presented by Mr. Thomas Mustaleski (right), President of the American Welding Society, to Mr. Shinsuke Tsutsumi (left)

Mr. Tsutsumi, as a member of the IIW Commissions II and XII, has contributed toward international standardization of welding consumables since 1991, when a draft of the ISO standard for flux-cored wires was first prepared by the IIW Commission XII. Since then the work of international standardization has had to encounter many turns and twists, involving hot arguments between a number of representatives from European countries, USA, Canada and Japan. In January 1998, however, at the ISO/TC44/SC3 (welding consumables) meeting, Mr. Tsutsumi proposed the " cohabitation idea ", as a way for two systems to" live together. "After the idea was accepted by ISO in 1999, progress on the international project of standardization has been boosted. The following cohabitation standards were published in 2002, which were prepared by the Japanese members in accordance with the consensus among the members from Canada, Japan and USA.

- (1) **ISO 14171**: SAW wires and wire-flux combinations for non alloy and fine grain steels
- (2) **ISO 14341**: GMAW wires for non alloy and fine grain steels

In addition, the final draft standards (ISO/FDIS 636, 17632, 17633, 17634, and 18276, for various welding consumables for carbon steel, low-alloy steel, and stainless steel) have been submitted to ISO/TC44/SC3 from Japan, which were prepared by the Subcommittee on ISO Standardization of the Technical Committee of the Welding Consumables Division of The Japan Welding Engineering Society. Mr. Tsutsumi has been engaged in such international activities as the Chair of the Subcommittee in Japan since 1998.

The Thomas Medal is awarded to an individual who has been involved in IIW/ISO international standards activities for more than ten years, and requires the presentation of a lecture that illustrates the incorporation of global studies in the standardization of welding technology. Thomas Medal Award has been given annually since 1998, and Mr. Tsutsumi received the 6th honor this year.



Thomas Medal: A prestigious honor that was denominated with the commemoration of the achievement of AWS standardization by Mr. Thomas and Dr. Thomas Jr. (USA)

Reported by KWT editorial staff

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